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SIMULATION PROGRAM FOR CENTRAL HELIUM LIQUEFIER

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ABSTRACT

The computer program described here analyzes the performance of Fermilab Central Helium Liquefier (CHL) and predicts the values of the plant thermodynamic variables at all process points in the plant. To simulate CHL, this program is modified from the prototype program which was developed by Hitachi Ltd. a couple of years ago. This program takes care of only the steady state simulation and takes account of the change of the turbine efficiency, the pressure drops and the UA values of the heat exchangers. How to use the program is shown in Appendix A.

PROGRAM DESCRIPTION

The principal program SHEREL is approximately 2000 FORTRAN statements including comments. SHEREL contains the main program and the subprograms, each of which takes care of the calculation for the corresponding component; i.e., the heat exchanger, the expansion turbine, the valve, the phase separators, etc. Figure 1 shows the flow diagram for CHL and the numbering used in the program. The components are connected by the linkage points. The main program controls the sequence of the calculation and manages the data at each linkage point and each flow path. Each component subprogram calculates the outlet process condition from the inlet process condition of its component at each iteration. Through the iteration the temperature values of the process points are changing automatically, and the iteration stops when it converges to the appropriate distribution which satisfies the heat and mass balance of the system and the restrictions demanded by the components.

In the subprogram for the heat exchanger, the differential equation for steady state heat transfer is solved by finite-difference method. The average value of helium specific heat is used at each flow path for reducing the calculation time. To prevent inaccuracy caused by this approximation, some heat exchangers are divided into a couple of smaller heat exchangers along the flow path.

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The capacity of the heat exchanger is the product of the overall heat transfer coefficient U and the area A , available for heat transfer. At the heat exchanger, A is constant and U mainly depends on the mass flow M . In the program the following expression is used for estimating the value of UA .^{1,2}

$$UA = (UA)_o (M/M_o)^{0.7}$$

Here, the suffix o means the design condition.

The pressure drop in the heat exchanger, ΔP , also depends on the mass flow M . The following similar expression is used in the program.

$$\Delta P = (\Delta P)_o (M/M_o)^{1.8}$$

In the subprogram for the valves, the following expressions about the coefficient of the valve C_v are used for calculating the relationship between the mass flow M and the pressure P .

$$\dot{M} = C_v \frac{\sqrt{P_1^2 - P_2^2}}{\sqrt{T}} \quad \text{at } P_2 \geq 0.5 P_1$$

$$\dot{M} = C_v \frac{P_1}{\sqrt{T}} \frac{\sqrt{3}}{2} \quad \text{at } P_2 \leq 0.5 P_1$$

(units: g/s, atm. K)

Here, T is the temperature and the suffix 1 and 2 represent the inlet and the outlet of the valve.

The program takes account of the change of the expansion turbine efficiency. A typical tendency of the expansion turbine efficiency corresponding to the velocity ratio is shown in Fig. 2.³ In the program, this diagram is approximated by the following expression.

$$\eta = \eta_{\max} \cos(u/C_o - \alpha)$$

Here, η is the efficiency of the expansion turbine, u is the rotor tip speed, C_o is the velocity equivalent of the adiabatic head and α is the value of u/C_o where the efficiency reaches the maximum.

The basis for the design of the plant is the TS diagram shown in Fig. 3. A total of approximately 1.0 g/s of helium flows out of the process through the labyrinth seals of the expansion turbines. The program neglects this flow which amounts to 0.07% of the design value of the compressor discharge.

APPLICATIONS

A sample of output from the program is shown in Appendix D. This output corresponds to the design condition. The output is displayed in the order of the sequence number of the components shown in Fig. 1. The linkage point number LN and the flow path number NF correspond to the numbers on Fig. 1.

As the first application, the influence on the J-T valve open rate is analyzed and the results are shown in Figs. 4-6. Figures 4 and 5 show the tendency of the flow rates at several flow paths and Fig. 6 shows the tendency of the temperature at several points corresponding to the open rate of the J-T valve. The C_v value corresponding to the design condition is about 90. The liquid helium production and liquid nitrogen consumption take maxima at around the design point.

As the second application, the performance of CHL is analyzed on the condition that the discharge pressure of the compressor is the same as design condition, 11.9 atm, and that the open rates of the J-T valve and the turbine #1 (T-1) inlet valve are changed. The J-T valve and T-1 valve are two main control valves in this system. The results are shown in Fig. 7. The curve A shows the helium production corresponding to the discharge flow rate of the compressor on the condition that the open rate of the T-1 inlet valve is constant and the open rate of J-T valve is changed. The other curves similar to curve A show the results in the case of the corresponding open rates of the T-1 inlet valve. The curve B shows the maximum helium production corresponding to the discharge flow rate of the compressor; that is the performance curve for CHL on this condition.

Another performance curve on condition that the discharge pressure of the compressor is 9.9 atm is shown in Fig. 8. From the comparison between Figs. 7 and 8, it is the best way to keep up the discharge flow rate of the compressor for producing the most liquid helium at the reduced operation mode.

The performance curve for another reduced operation is shown in Fig. 9. In this case, the discharge pressure is 11.9 atm, the design pressure, but the turbine #2 inlet valve is closed or the turbine #2 is isolated from the process line. The liquid helium production decreases remarkably.

ACKNOWLEDGEMENTS

I would like to thank Drs. R.Walker, G.Mulholland, H.Barton, W.Fowler and R.Yamada for their advice on this work and the hospitality extended during my stay at Fermilab.

REFERENCE

1. Kays, W.M., and A.L. London; "Compact Heat Exchangers," 2nd ed., McGraw-Hill Book Company, New York, 1964.
2. Barton, H.R., J.E.Nichols, and G.T.Mulholland; "Satellite I: Model for the Satellite Mode Refrigerator," TM-984, 1980.
3. Haselden, G.G.; "Cryogenic Fundamentals," Academic Press, London, 1971.

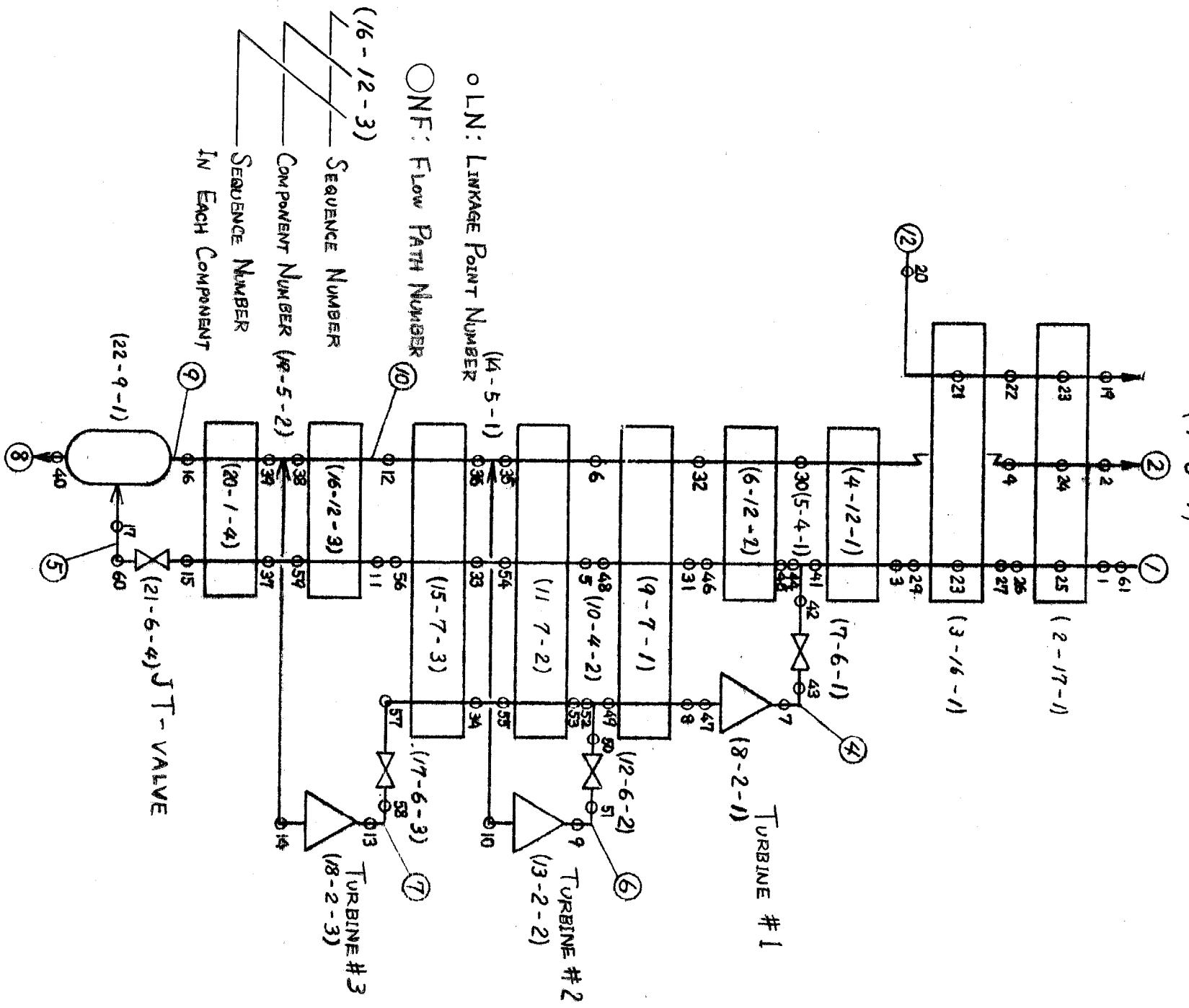


FIGURE 1

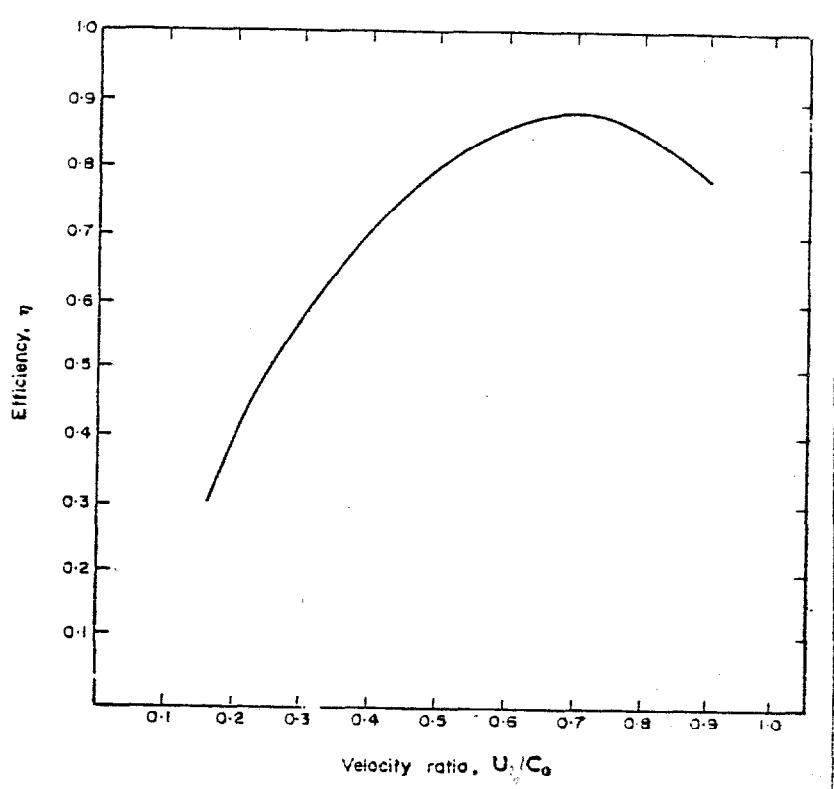


FIGURE 2

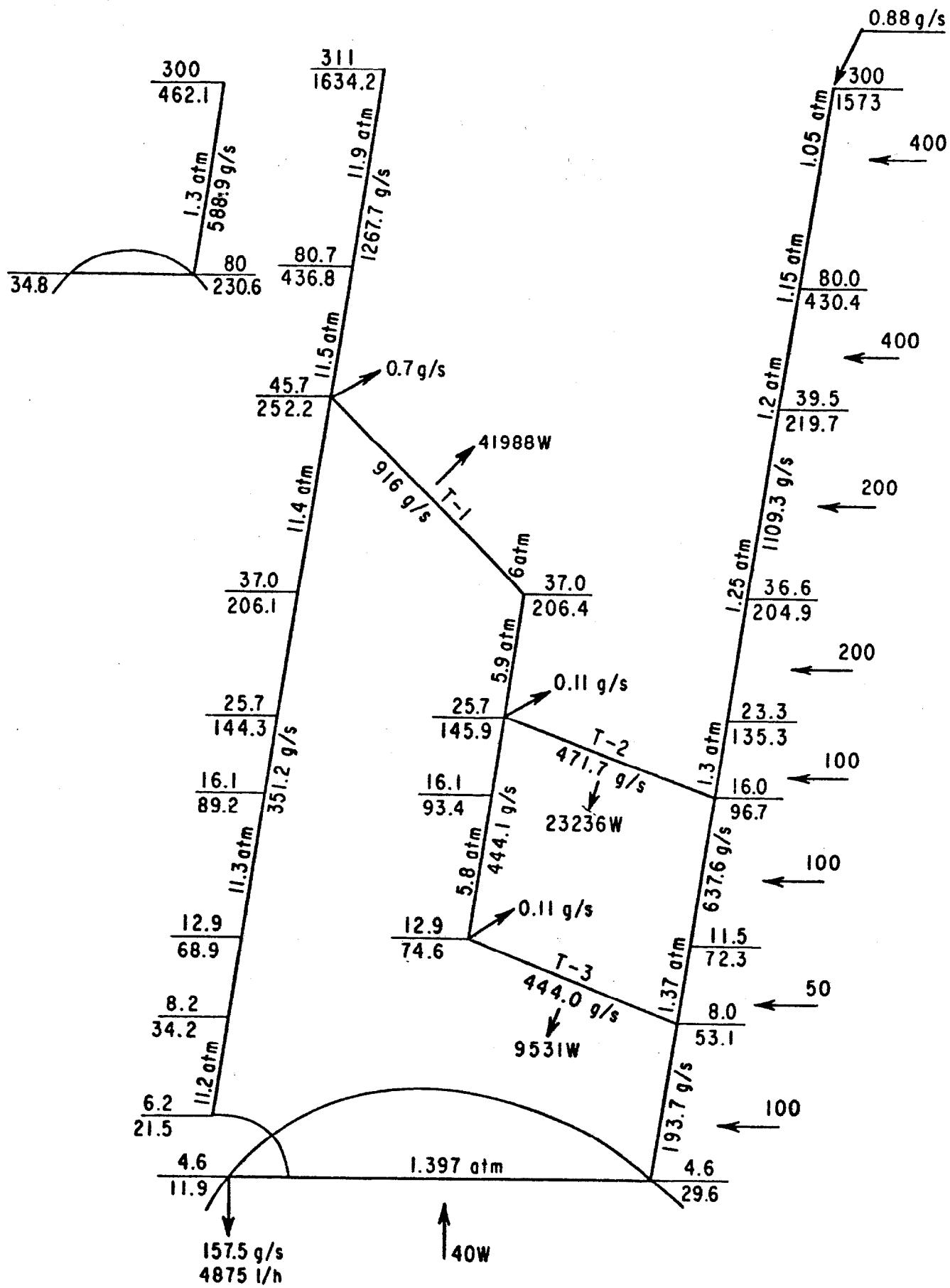
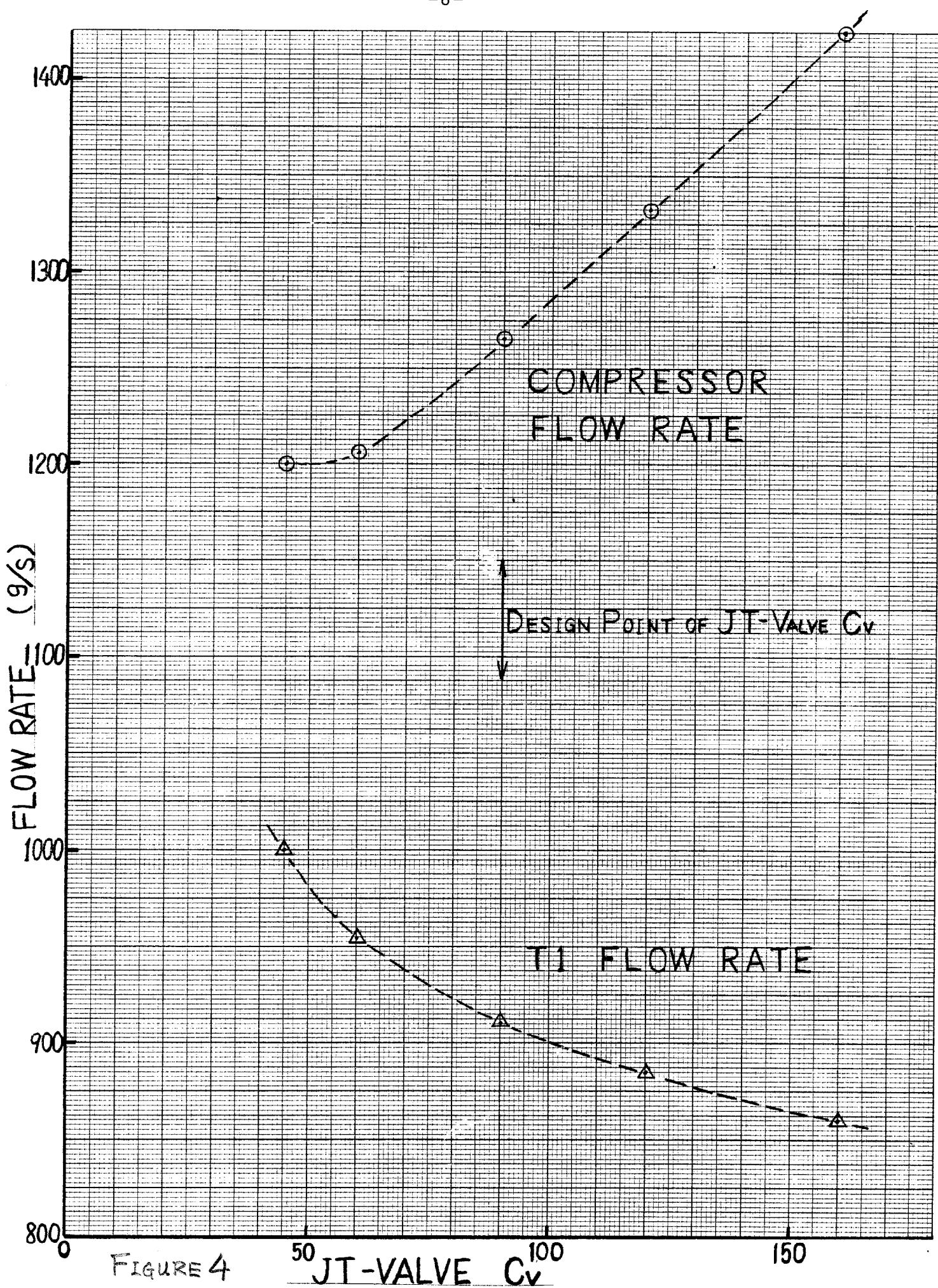


FIGURE 3



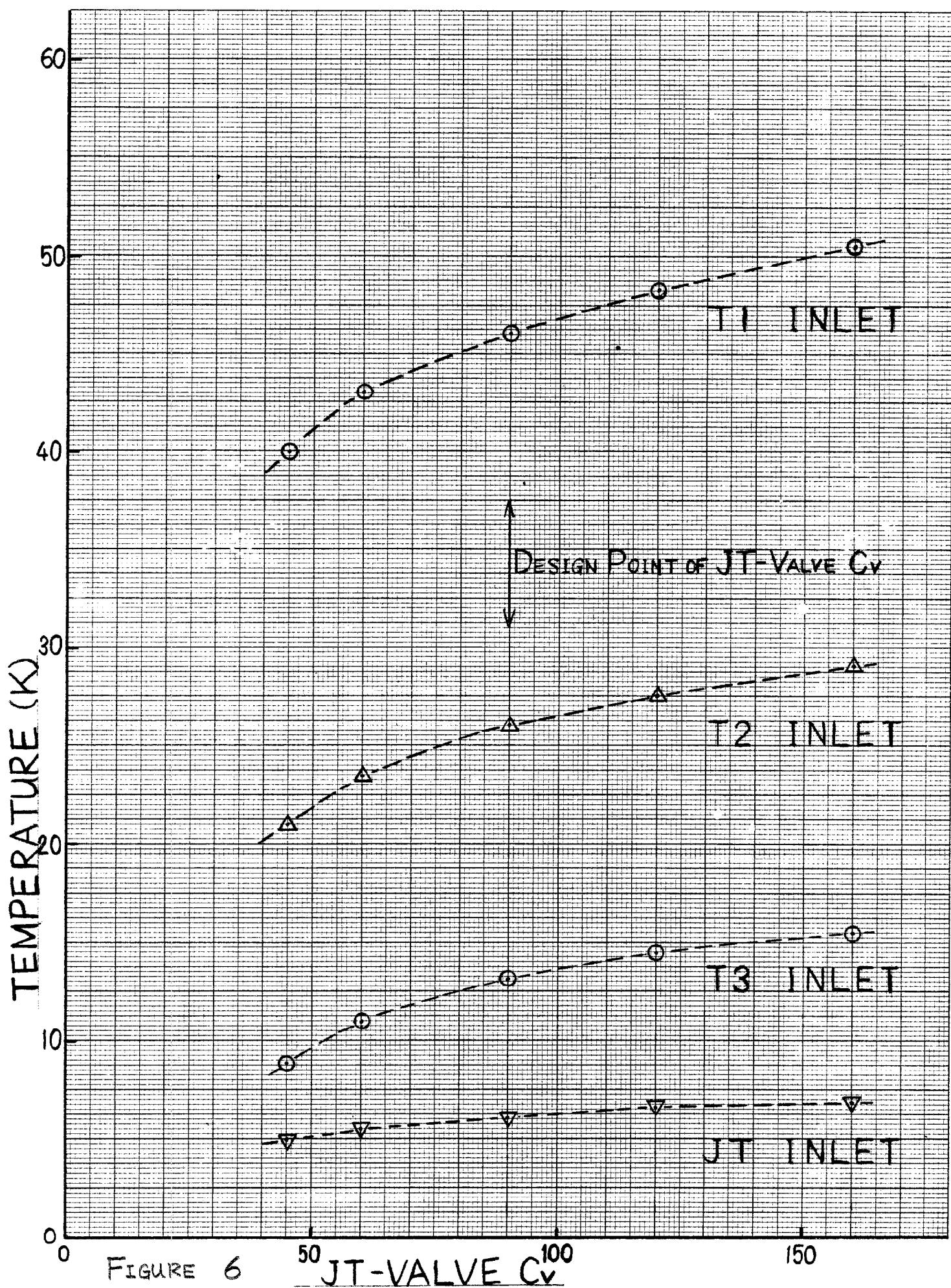
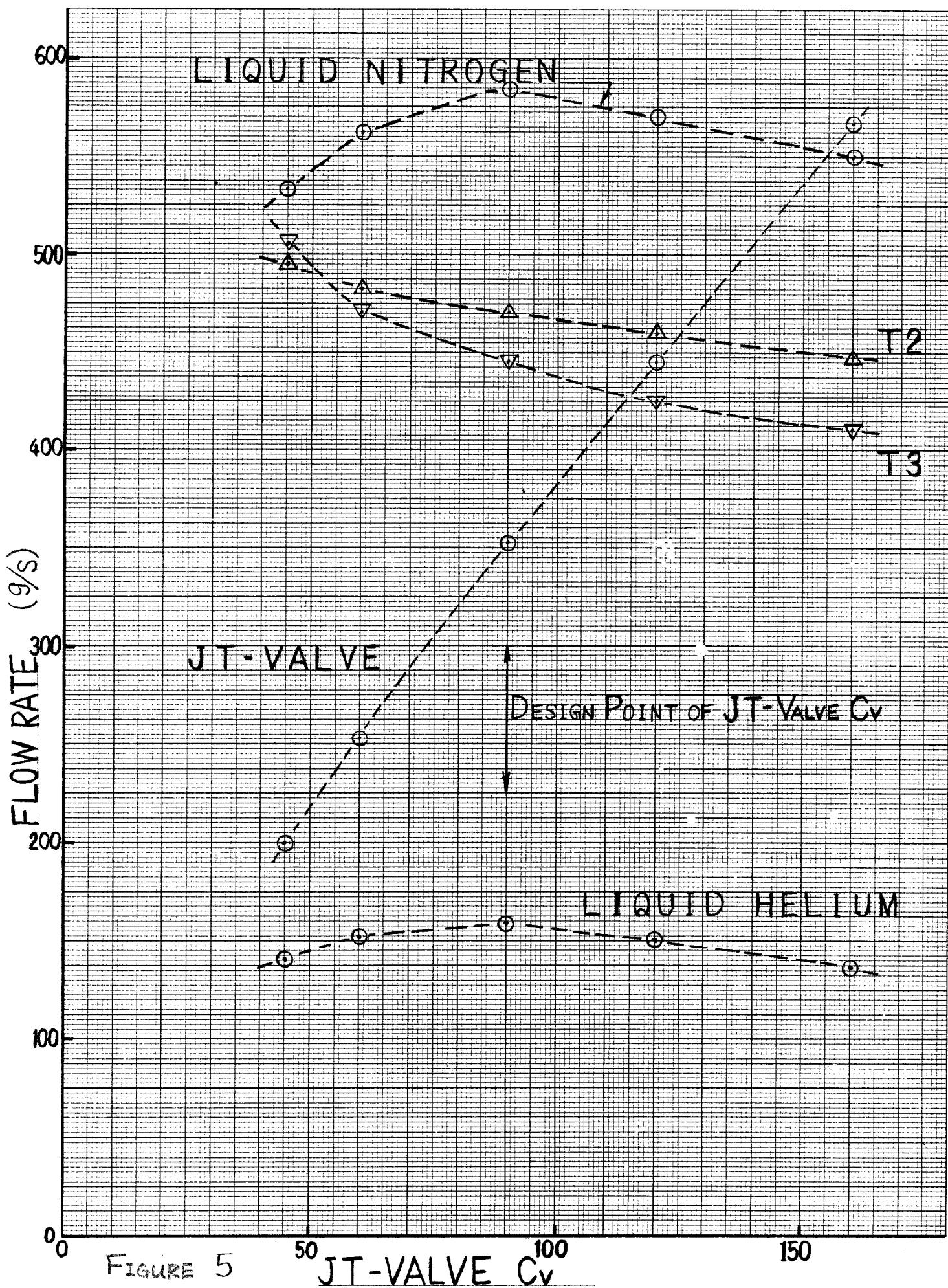


FIGURE 6



LIQUEFACTION CAPACITY (g/s)

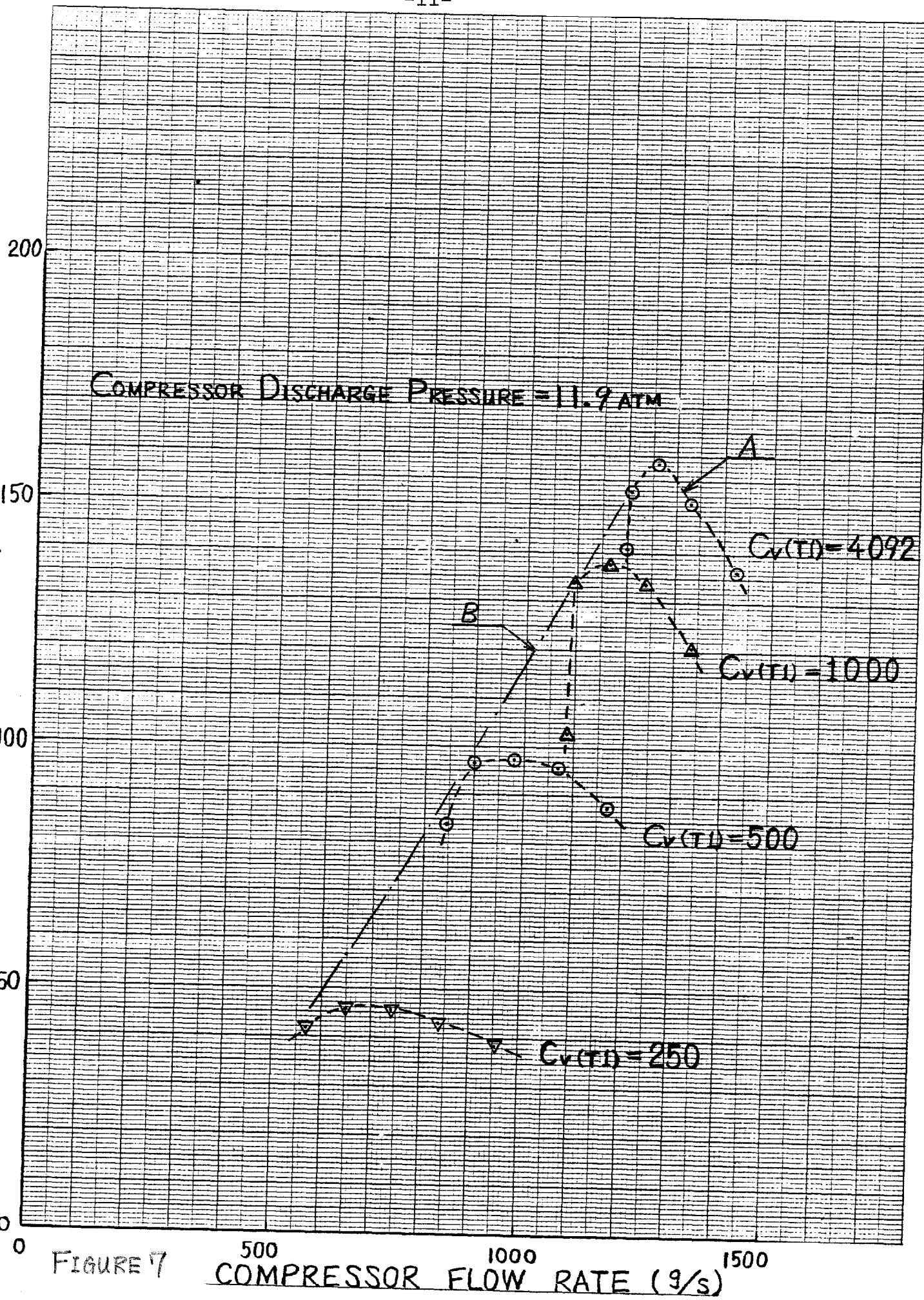
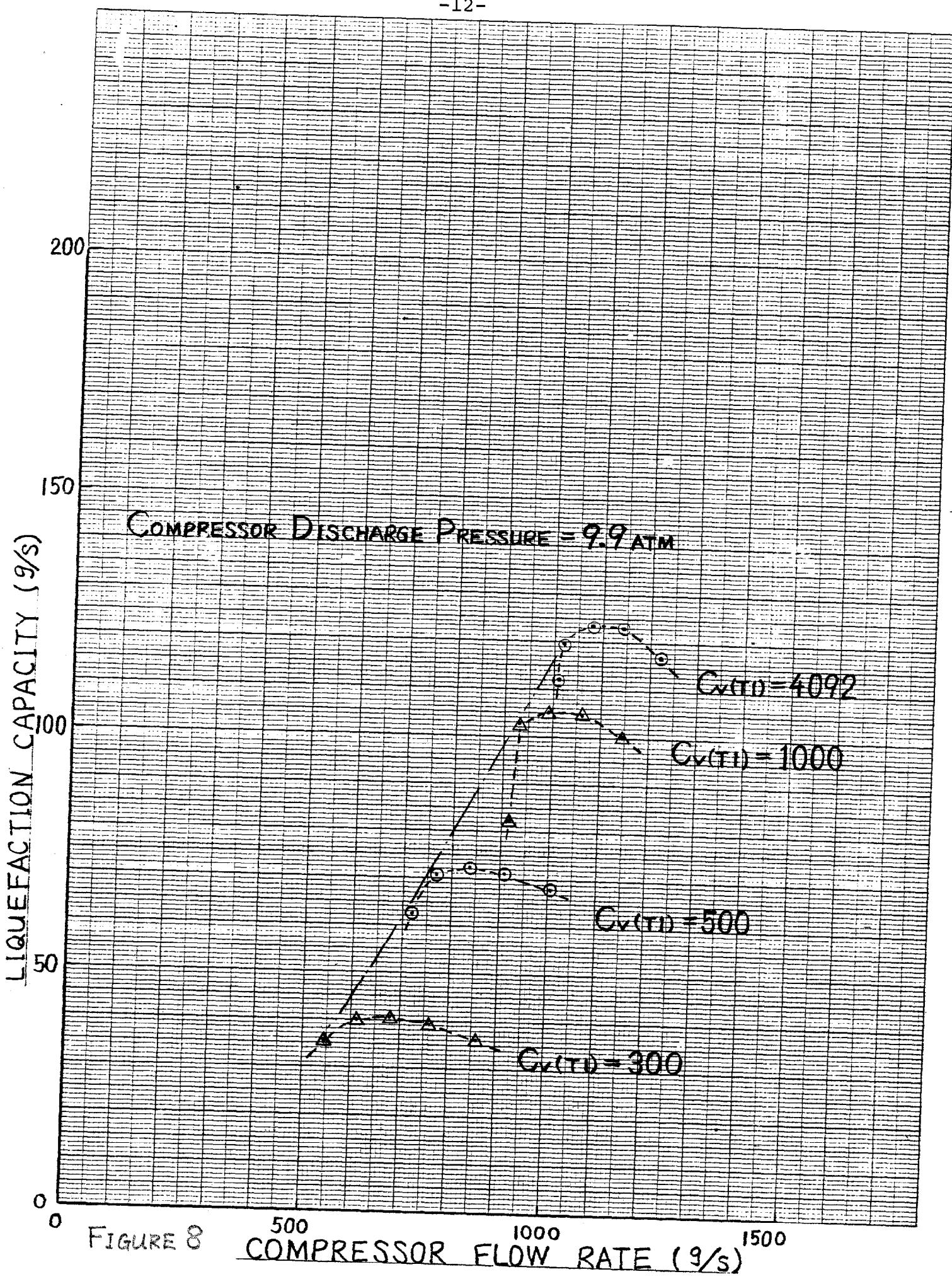
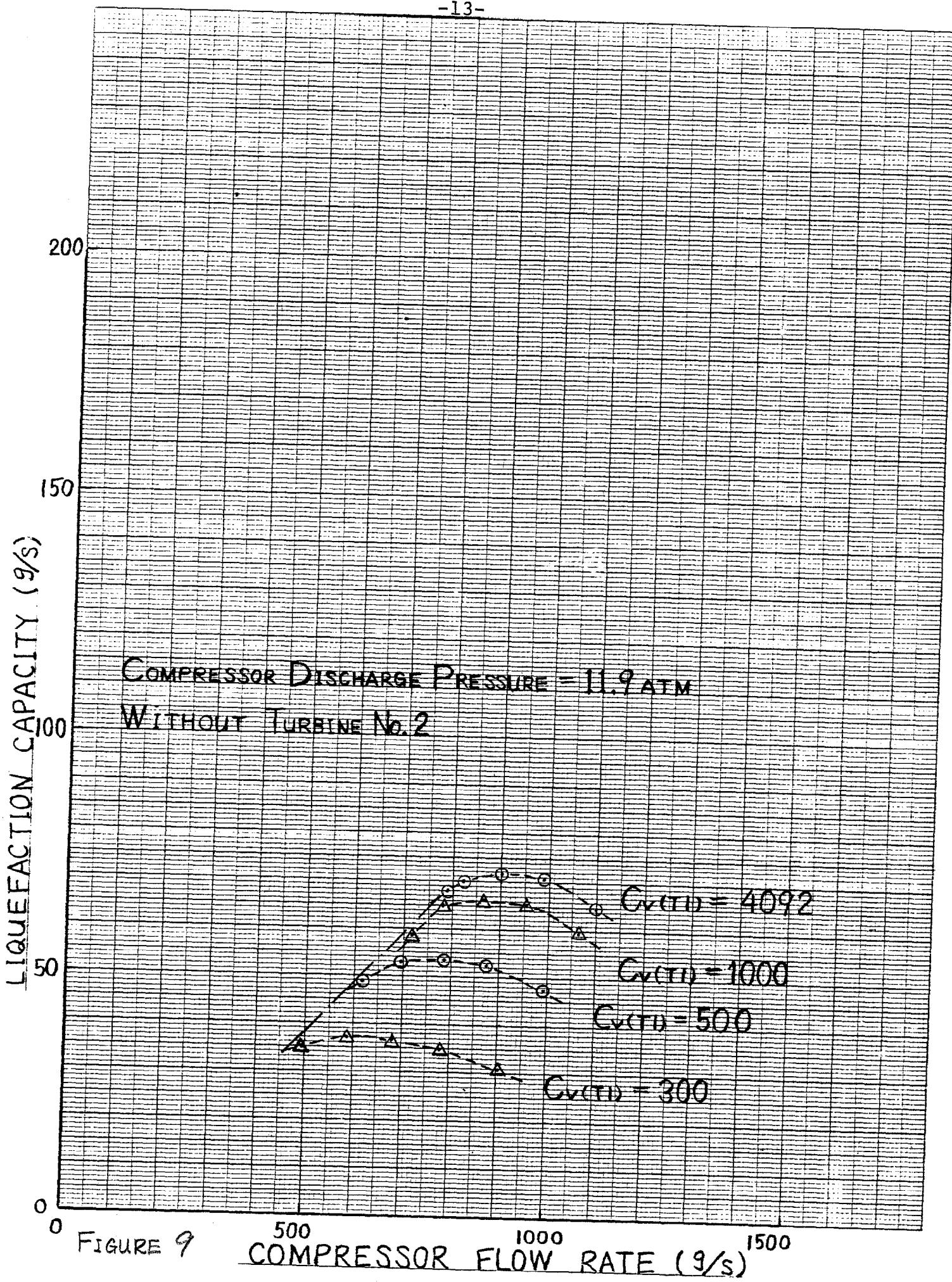


FIGURE 7

COMPRESSOR FLOW RATE (g/s)





APPENDIX A

HOW TO USE THE SIMULATION PROGRAM FOR CHL

1. Starting up.

- a. Log in.
- b. Type the following commands:

```
/GET,HEREF/UN=V3055  
/GET,ELMDATA/UN=V3055  
/GET,INTDATA/UN=V3055  
/HEREF
```

HEREF is a procedure program which contains the commands for transferring the permanent files to the local files, compiling, linking and executing the several kinds of programs. ELMDATA contains information about the refrigeration equipment and the linkage relationship among the equipment. A sample ELMDATA is shown in Appendix B. INTDATA contains the initial data of pressure, temperature, and enthalpy at each linkage point and the data of flow rate at each flow path. A sample INTDATA is shown in Appendix C. It takes a few minutes to start the calculation.

2. Printing the results.

When the calculation is completed without errors, "NORMAL END" appears on the terminal. The result of the calculation is written in a local file called ROUTPUT. To print ROUTPUT, type

```
/R,ROUTPUT  
/ROUTE,ROUTPUT,DC=PR
```

3. Rerun.

To rerun the program with the same INTDATA that was used at the previous run, type

```
/HEREFR
```

4. Continuation of the run.

When the number of repetition of the calculation reaches the specified limit (default: 100 cycles) but the temperature distribution does not converge, the following message appears on the screen:

"THE CALCULATION IS NOW ON THE REPETITION LIMIT. PLEASE TYPE (HEREFC) TO CONTINUE THE CALCULATION."

To continue the calculation, type

```
/HEREFC
```

5. Time limit.

When the program does not get to the end in the time limit specified by the computer "TIME LIMIT" appears on the screen. To terminate the run, type

/"CTRL" + T

then reduce the number of repetition limit of the local file ELMDATA. To rerun the program, type

/HEREFR

6. Post-mortem dump.

In case of a fatal computation error, a post-mortem dump will be generated on the file PMDUMP. To examine this dump, type

/R,PMDUMP
/C,PMDUMP

7. Change ELMDATA and/or INTDATA.

To edit the data of ELMDATA and/or INTDATA, use ICE.

APPENDIX B

ELM DATA								
24	100	0	2					
0.01	0.6	0.7	1.8					
8	1							
1267.7	1.05	0.04	11.9	311.0	0.0	0.0	0.0	0.0
2	61							
2	1							
4	6	1	2	1	43			
6	6	2	2	2	51			
7	6	3	2	3	58			
11	0	6	0	7	0			
5	6	4	0	0	0			
1	0	4	0	5	0			
9	0	2	-1	8	0			
10	0	7	0	9	0			
2	0	6	0	10	0			
0	0	0	0	0	0			
17	1							
300.0	9309.0	89022.0	588.9	1109.3	1267.7	0.0	0.06	
0.1								
19	22	2	4	1	26	61	23	
24	25							
12	2	1						
16	1							
100.0	21576.0	588.9	1267.7	0.0	0.1			
22	20	27	29	26	21	29		
12	1							
12	1							
400.0	93849.0	1109.3	1267.7	0.05	0.2			
4	30	3	41	29				
2	1							
0	65							
4	1							
0.0								
41	42	44						
1	4	5						
12	2							
200.0	8238.0	1109.3	351.2	0.	0.1			
30	32	45	46	44				
2	5							
0	75							
6	1							
0.0	4092.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0
42	43							
4								
2	1							
0.829	638.83	0.7	0.0	0.0	0.0	0.0	0.0	42195.7
233.135	0.829	229.44	270.93					
7	47	43						
7	1							
200.0	0.0	22045.2	54432.5	1109.3	351.2	916.0	0.05	
0.1	0.1							
32	6	31	48	8	49	46	47	
2	5	4						
4	2							
0.0								
49	50	52						
11	6	7						
7	2							
100.0	0.0	31126.7	36425.2	1109.3	351.2	444.0	0.05	
0.	0.1							
6	35	5	54	53	55	48	52	
2		7						

APPENDIX C

INTDATA						
1						
11.9	311.0	1634.2	1.25	36.6	204.9	3
2			33	16.1	89.2	0.0
1.05	300.0	1573.0	34	16.1	93.4	4
3			35	16.0	96.7	916.0
11.7	80.7	436.8	1.3	16.0	96.7	5
4			36	16.0	96.7	351.2
1.15	80.0	430.4	1.3	16.0	96.7	6
5			37	8.2	34.2	471.7
11.4	25.7	144.3	1.2	8.0	53.1	7
6			38	8.0	53.1	444.0
1.3	23.3	135.3	1.37	8.0	53.1	8
7			39	8.0	53.1	157.5
11.5	45.7	252.2	1.37	8.0	53.1	9
8			40	4.6	11.9	193.7
6.0	37.0	206.4	1.397	4.6	11.9	10
9			41	11.5	252.2	637.6
5.9	25.7	145.9	11.5	45.7	252.2	11
10			42	45.7	252.2	916.0
1.3	16.0	96.7	11.5	45.7	252.2	12
11			43	45.7	252.2	588.9
11.3	12.9	68.9	11.5	45.7	252.2	0
12			44			
1.37	11.5	72.3	11.5	45.7	252.2	
13			45			
5.8	12.9	74.6	11.5	45.7	252.2	
14			46			
1.37	8.0	53.1	11.4	37.0	206.1	
15			47			
11.2	6.2	21.5	6.0	37.0	206.4	
16			48			
1.397	4.6	29.6	11.4	25.7	144.3	
17			49			
1.397	4.6	21.5	5.0	25.7	145.9	
18			5.0			
0.0	0.0	0.0	5.9	25.7	145.9	
19			51			
1.3	300.0	311.1	5.9	25.7	145.9	
20			52			
1.3	79.66	-116.62	5.9	25.7	145.9	
21			53			
1.3	79.66	78.934	5.9	25.7	145.9	
22			54			
1.3	79.66	78.934	11.3	16.1	89.2	
23			55			
1.3	79.66	78.934	5.8	16.1	93.4	
24			56			
1.15	80.0	430.4	11.3	12.9	68.9	
25			57			
11.8	98.09	526.66	5.8	12.0	74.6	
26			58			
11.8	98.09	526.66	5.8	12.0	74.6	
27			59			
11.8	98.09	526.66	11.2	8.2	34.2	
28			60			
11.8	98.09	526.66	1.397	4.6	21.5	
29			61			
11.7	80.7	430.8	11.9	311.0	1034.2	
30			0			
1.2	39.5	219.7	1			
31			267.7			
1.4	37.0	205.1	2			
32			1409.3			

NORMAL END

ELMDATA=ELMDATA

INTDATA=INTDATA

REPETITION NO.= 33

SUMMATION OF DELT.TEMP.= .00923

DMIT= .01000 RAMD= .60000 AUEXP= .70000 DPEXP=1.80000

NO= 1 8(FLOW CONT) NO= 1
FLOW.MAX PRESS.SUC DP.SUC PRESS.DISCH TEMP.DISCH

1267.70000 1.05000 .04000 11.90000 311.00000 0.00000 0.00000 0.00000

NO= 2 17(NX21) NO= 1
QL AU13D AU23D F1D F2D F3D DP1D DP2D

300.00000 9309.00000 89022.00000 588.90000 1109.30000 1267.70000 0.00000 .06000

DP3D AU13 AU23 DP1 DP2 DP3
.16000 9281.07798 88863.65654 0.00000 .05969 .09960

NO	FLOW NO	FLOW RATE F(G/S)	***** HOT END *****			***** COLD END *****				
			LN	P(ATM)	T(K)	H(J/G)	LN	P(ATM)	T(K)	H(J/G)
1	12	585.1657	19	1.3000	300.0053	311.0913	22	1.3000	99.9317	101.3978
2	2	1106.1049	2	1.0900	300.2517	1574.2584	4	1.1497	80.2342	431.5442
3	1	1264.9116	1	11.9000	311.0000	1634.2000	26	11.8004	100.2373	538.1763

NO= 3 16(NX11) NO= 1
QL AU13D F1D F2D DP1D DP2D DP1

100.00000 21576.00000 588.90000 1267.70000 0.00000 .16000 21511.28354 0.00000

DP2
.09960

NO	FLOW NO	FLOW RATE F(G/S)	***** HOT END *****			***** COLD END *****				
			LN	P(ATM)	T(K)	H(J/G)	LN	P(ATM)	T(K)	H(J/G)
1	12	585.1657	22	1.3000	99.9317	101.3978	20	1.3000	79.4269	-116.8717
2	1	1264.9116	27	11.8004	100.2373	538.1763	29	11.7008	80.0957	437.2751

NO= 4 12(HX11-DIV) NO= 1
QL AU13 F1D F2D DP1D DP2D DP1

400.00000 93849.00000 1109.30000 1267.70000 0.05000 .20000 93682.07075 0.04974

DP2
.19921NO.DIV LNSTART
0 65

NO	FLOW NO	FLOW RATE F(G/S)	***** HOT END *****			***** COLD END *****				
			LN	P(ATM)	T(K)	H(J/G)	LN	P(ATM)	T(K)	H(J/G)
1	2	1106.1049	4	1.1497	80.2342	431.5442	30	1.1994	40.0804	222.7608
2	1	1264.9116	3	11.7008	80.0957	437.2751	41	11.5016	46.1921	255.0114

NO= 5 4(FLOW SEPR) NO= 1
0.00000

NO= 6 12(HX11-DIV) NO= 2

200.00000 AU13 8238.00000 1109.30000 F2D DP1D
 0.00000 351.20000 .10000 8256.48852 0.00000
 DP2
 *10169
 NO.DIV LNSTART
 0 75

NO FLOW NO FLOW RATE ****END**** COLD END ***
 F(G/S) LN P(ATM) T(K) H(J/G)
 1 2 1106.1049 1.1994 40.0804 22.7658 LN P(ATM) T(K) H(J/G)
 2 5 354.4869 1.5016 46.1921 255.0114 32 1.1994 37.2117 207.8180
 45
 NO= 7 QL 6(VALVE CV) NO= 1
 0.00000 4092.00000 0.00000 0.00000 2041.88056 BETAA2 PRESSIN
 0.00000 11.50158 11.40174 42195.70000

NO FLOW NO FLOW RATE ****END**** COLD END ***
 F(G/S) LN P(ATM) T(K) H(J/G)
 1 4 910.4247 1.5016 46.1921 255.0114 LN P(ATM) T(K) H(J/G)
 42
 NO= 8 EFFICID CV) NO= 1 TU/C00D DELT.ENTH. WORK ****END**** COLD END ***
 .82900 638.83000 .70000 45.83060 41725.30655 BETAA2 PRESSIN
 1.00000 233.13500 .82900 229.44000 U.HIGH 94.00525 11.40174 42195.70000

NO FLOW NO FLOW RATE ****END**** COLD END ***
 F(G/S) LN P(ATM) T(K) H(J/G)
 1 4 910.4247 1.4017 46.1813 255.0114 LN P(ATM) T(K) H(J/G)
 7
 NO= 9 QL 7(HX12) NO= 1 AU13D ****END**** COLD END ***
 0.00000 22045.20000 54432.50000 1109.30000 F1D F40 DP1D
 200.00000 0.00000 22045.20000 54432.50000 351.20000 916.00000 .05000
 DP3D
 100000 0.10000 22094.67598 AU13 AU14 DP1 0.4974 DP4
 .10169 .09891

NO FLOW NO FLOW RATE ****END**** COLD END ***
 F(G/S) LN P(ATM) T(K) H(J/G)
 1 2 1106.1049 1.1994 37.2117 207.8180 LN P(ATM) T(K) H(J/G)
 2 5 354.4869 1.3992 37.5451 208.9271 6 1.2492 23.7189 137.3468
 4 4 910.4247 1.0172 37.5243 209.1474 49 1.2982 26.0191 146.2987
 NO=10 4(FLOW SEPR) NO= 2

NO=11 QL 7(HX12) NO= 2 AU13D ****END**** COLD END ***
 100.00000 0.00000 31126.70000 36425.20000 1109.30000 F1D F4D DP1D
 0.00000 DP40 AU13 AU14 DP1 0.4974 DP4 .05000
 .10000 31196.55756 36286.90554 0.00000 .09857

NO FLOW NO FLOW RATE ****END**** COLD END ***
 F(G/S) LN P(ATM) T(K) H(J/G) LN P(ATM) T(K) H(J/G)

1	2	5	1106.1049	6	1.2492	23.7189	137.3468	35	1.2989	16.2805	98.1517				
2	3	7	354.4869	53	11.2982	26.0191	146.2987	54	11.2982	16.3500	90.6409				
3	4	6	440.4713	53	5.9183	26.0684	148.1515	55	5.8197	16.3518	94.7369				
NO=12 6 (VALVE) NO= 2				BETA1 1053.36573 BETA2 432.99427 PRESS.IN 5.91826				0.00000							
1	2	3	4	5	6	7	8	9	10	11	12				
NO	FLOW	NO	FLOW RATE	F(G/S)	LN	P(ATM)	HOT	END	LN	P(ATM)	COLD				
1	6	469.9579	.82100	476.07000	50	5.9183	26.0684	148.1515	51	5.8179	T(K) H(J/G)				
NO=13 2 (TURBINE) NO= 2				DELT.ENTH. 49.95467 WORK 23476.59172 BETA2 93.27310 PRESS.IN 5.81792				WORK.D 23470.30000							
1	2	3	4	5	6	7	8	9	10	11	12				
EFFIC.D	CV	(U/COLD	U.COOL	U.COOL	U.COOL	U.COOL	U.COOL	U.COOL	U.COOL	U.COOL	U.COOL				
.82100	476.07000	.70000	49.95467	23476.59172	93.27310	5.81792	23470.30000								
U.D	EFFIC.	U.LOW	U.HIGH												
244.20000	.82100	231.38000	305.23000												
1	2	3	4	5	6	7	8	9	10	11	12				
NO	FLOW	NO	FLOW RATE	F(G/S)	LN	P(ATM)	HOT	END	LN	P(ATM)	COLD				
1	6	469.9579	.82100	476.07000	9	5.8179	26.0513	148.1515	10	1.2989	T(K) H(J/G)				
NO=14 5 (FLOW SUM) NO= 1				0.00000				16.2885 98.1940							
1	2	3	4	5	6	7	8	9	10	11	12				
NO=15 7 (HX12) NO= 3				AU13D 14478.00000 AU14D 18367.20000 F1D 637.60000 F3D 351.20000 F4D 444.00000 DP1D 0.00000											
1	2	3	4	5	6	7	8	9	10	11	12				
QL2	QL3	AU13D	AU14D	F1D	F3D	F4D	DP1D	DP2D	DP3D	DP4D	DP5D				
100.00000	0.00000	14478.00000	18367.20000	637.60000	351.20000	444.00000	0.00000	0.00000	0.00000	0.00000	0.00000				
DP3D	DP4D	AU13	AU14	DP1	DP3	DP4									
0.00000	0.00000	14513.56838	18301.32051	0.00000	0.00000	0.00000									
1	2	3	4	5	6	7	8	9	10	11	12				
NO	FLOW	NO	FLOW RATE	F(G/S)	LN	P(ATM)	HOT	END	LN	P(ATM)	COLD				
1	2	3	4	5	6	7	8	9	10	11	12				
636.1470	354.4869	440.4713	636.1470	354.4869	440.4713	1.2989	1.2989	1.2989	1.2989	1.2989	1.2989				
10	11	12	13	14	15	16	17	18	19	20	21				
1.2989	11.2982	11.2982	11.2982	11.2982	11.2982	16.2748	16.3500	16.3518	98.1214	90.6409	94.7369				
16.2748	16.3500	16.3518	16.3518	16.3518	16.3518	98.1214	90.6409	94.7369	11.9110	11.3058	13.2219				
98.1214	90.6409	94.7369	94.7369	94.7369	94.7369	11.9110	11.3058	13.2219	74.8114	71.6516	76.5787				
NO=16 12 (HX11-DIV) NO= 3				AU13 29759.00000 F1D 637.60000 F2D 351.20000 DP1D .06000 DP2D .10000 DP3D .05975											
1	2	3	4	5	6	7	8	9	10	11	12				
DP2	DP3	DP4	DP5	DP6	DP7	DP8	DP9	DP10	DP11	DP12	DP13				
.10169															
NO.DIV	LNSTART														
1	85														
1	2	3	4	5	6	7	8	9	10	11	12				
NO	FLOW	NO	FLOW RATE	F(G/S)	LN	P(ATM)	HOT	END	LN	P(ATM)	COLD				
1	2	3	4	5	6	7	8	9	10	11	12				
636.1470	354.4869	440.4713	636.1470	354.4869	440.4713	1.2989	1.2989	1.2989	1.2989	1.2989	1.2989				
10	11	12	13	14	15	16	17	18	19	20	21				
1.2989	11.2982	11.2982	11.2982	11.2982	11.2982	11.9110	13.3058	13.3058	74.8114	71.6516	76.5787				
11.9110	13.3058	13.3058	13.3058	13.3058	13.3058	74.8114	71.6516	76.5787	8.1576	8.2646	34.6072				
NO=17 6 (VALVE) NO= 3				BETA1 985.57624 BETA2 408.96003 PRESS.IN 5.81969				0.00000							
1	2	3	4	5	6	7	8	9	10	11	12				
QL	CV	0.00000	1487.06000	0.00000	0.00000	BETA1	BETA2	PRESS.IN	0.00000						

NO	FLOW NO	FLOW RATE F(G/S)	HOT			COLD			
			LN	P(ATM)	T(K)	LN	P(ATM)	T(K)	
1	7	440.4713	57	5.8197	13.2219	76.5787	58	5.7192	13.1958

NO=18 2(TURBINE) NO= 3
 EFFIC.D CV (U/CD)D DELT.ENTH. WORK BETA2 PRESS.IN WORK.D
 .81300 323.05000 .70000 22.46045 9893.18191 88.93075 5.71918 9525.10000
 U.D EFFIC. U.LIN U.HIGH
 161.10000 .81293 129.12000 255.49000

NO	FLOW NO	FLOW RATE F(G/S)	HOT			COLD			
			LN	P(ATM)	T(K)	LN	P(ATM)	T(K)	
1	7	440.4713	13	5.7192	13.1958	76.5787	14	1.3288	8.1623

NO=19 5(FLOW SUM) NO= 2
 0.00000

NO=20 12(HX11-DIV) NO= 4
 QL AU13 F1D F2D DP1D DP2D AU13 DP1
 100.00000 6679.00000 193.70000 351.20000 .03800 0.00000 6724.65451 .03870

DP2
 0.00000

NO	FLOW NO	FLOW RATE F(G/S)	HOT			COLD			
			LN	P(ATM)	T(K)	LN	P(ATM)	T(K)	
1	9	195.6758	39	1.3288	8.1469	54.0305	16	1.3481	4.5555

2	5	354.4869	37	11.2474	8.2646	34.6072	15	11.2474	6.1371
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NO=21 6(VALVE) NO= 4
 QL CV 0.00000 90.15700 0.00000 0.00000 BETA1 BETA2 PRESS.IN
 0.00000 0.00000 0.00000 0.00000 122.05187 36.39311 11.24735 0.00000

NO	FLOW NO	FLOW RATE F(G/S)	HOT			COLD			
			LN	P(ATM)	T(K)	LN	P(ATM)	T(K)	
1	5	354.4869	15	11.2474	6.1371	21.4649	60	1.3481	4.5555

NO=22 9(LIQ SEPRT) NO= 1
 QL QRD QR FLOW.LIQ
 40.00000 0.00000 0.00000 158.81112

NO=23 18(CONTROLLER) NO= 1
 NO MEASUR. CNTRL.ELM
 19 TEMP. FLOW NO.
 NO. 12

TARGET	P-COEFF.	I-COEFF.	D-COEFF.	1-BEFORE	2-BEFORE	3-BEFORE	4-BEFORE
300.00000	1.00000	.50000	.50000	.00529	.00537	.00542	.00542

NO=24 18(CONTROLLER) NO= 2
 NO MEASUR. CNTRL.ELM
 11 FLOW PRESS. NO.
 NO. 47

TARGET	P-COEFF	I-COEFF	D-COEFF	1-BEFORE	2-BEFORE	3-BEFORE	4-BEFORE
4.00000	-.00500	-.00100	-.00100	.00452	.00521	.00594	.00654
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